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NASA CR-

147847

SPACE SHUTTLE ENGINEERING AND OPERATIONS SUPPORT

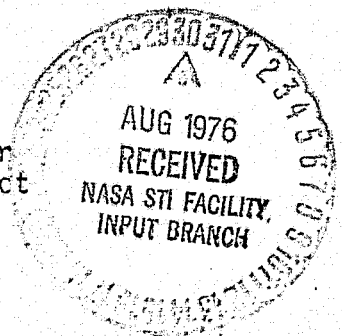
DESIGN NOTE NO. 1.4-2-7

STAR TRACKER CONSTRAINT VIOLATIONS DIGITAL CAPABILITY  
DESCRIPTION AND ANALYSIS RESULTS

MISSION PLANNING, MISSION ANALYSIS AND SOFTWARE FORMULATION

30 January 1975

This Design Note is Submitted to NASA Under Task Order  
No. D0102, Subtask 2, Task Assignment 1.4-2-B, Contract  
NAS-9-13970



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N76-29349  
HC 44.00  
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48422  
32 p G3/17  
(NASA-CR-147847) STAR TRACKER CONSTRAINT  
VIOLATIONS DIGITAL CAPABILITY DESCRIPTION  
AND ANALYSIS RESULTS. MISSION PLANNING,  
MISSION ANALYSIS, AND SOFTWARE FORMULATION  
(McDonnell-Douglas Technical Services)

## 1.0 SUMMARY

Results of star tracker constraint violation analyses performed with the digital computer program Shuttle Attitude and Pointing Time Line Processor (SAPT) are presented in this note. These analysis results are typical of those utilized to provide the information required to update Baseline Reference Mission Attitude and Pointing Time Lines. Descriptions of SAPT modifications implemented to perform these analyses are also presented.

## 2.0 INTRODUCTION

The purpose of this note is to present results of star tracker constraint violation analyses and to document and discuss the associated modifications to Program SAPT designed to detect star tracker constraint violations. This note, therefore, describes and documents a tool which may be utilized to analyze attitude and pointing time lines, now and in the future, for possible star tracker constraint violations. This capability has been utilized to perform initial analyses which are reflected in the time lines presented in References (1) and (2). This capability and other simulation requirements designed to support attitude profile analyses are discussed briefly in Reference (3).

## 3.0 DISCUSSION

The orbiter vehicle has three star trackers. Each is sensitive to bright light and cannot be operated within certain regions of the sun or sunlit earth. Attempting to operate any one of the star

trackers with its centerline Field of View (FOV) within 30 degrees of the sun or within 20 degrees of the sunlit earth horizon would violate operational constraints imposed on this instrument. Violations may occur while performing Inertial Measurement Unit (IMU) platform alinements or while tracking targets during normal Shuttle activities. This condition in certain cases can be avoided by selecting alternate orbiter attitudes, and a method to detect these violations can be useful in establishing a pre-mission attitude and pointing profile.

Consideration was given to developing a separate program to determine the constraint violations, but it was determined that Program SAPT would be the most convenient tool with which to perform the violation analyses. There are three main reasons why this is the case. First, Program SAPT generates the attitude and pointing time line profiles and contains all of the attitude related information required to establish the necessary attitude transformation relationships. Second, the program can be easily modified, and third, the program employs routines required for certain computations associated with the star tracker constraint violation model.

#### 4.0 RESULTS

Figure 1 depicts the earth pointing constraint detection model implemented in Program SAPT. It assumes the earth is a sphere. Since the earth is assumed to be spherical, the angle,  $\alpha$ , between the vehicle to earth-tangent line and vehicle to earth-center line will be constant if

the vehicle's altitude remains constant, i.e., if the vehicle's orbit is circular. The earth pointing constraint is violated when the angle between the star tracker FOV centerline and the vehicle to earth centerline,  $\theta$ , decreases below the value of  $\alpha + 20^\circ$ . This is equivalent to the star tracker centerline FOV entering the earth pointing constraint region and, therefore, violating the earth pointing constraint. The sun constraint detection model is implemented in a similar manner. The sun is regarded as a point source, and sun pointing constraints are violated when the star tracker centerline FOV enters within 30 degrees of the sun to vehicle line.

Program SAPT was modified to incorporate this model.

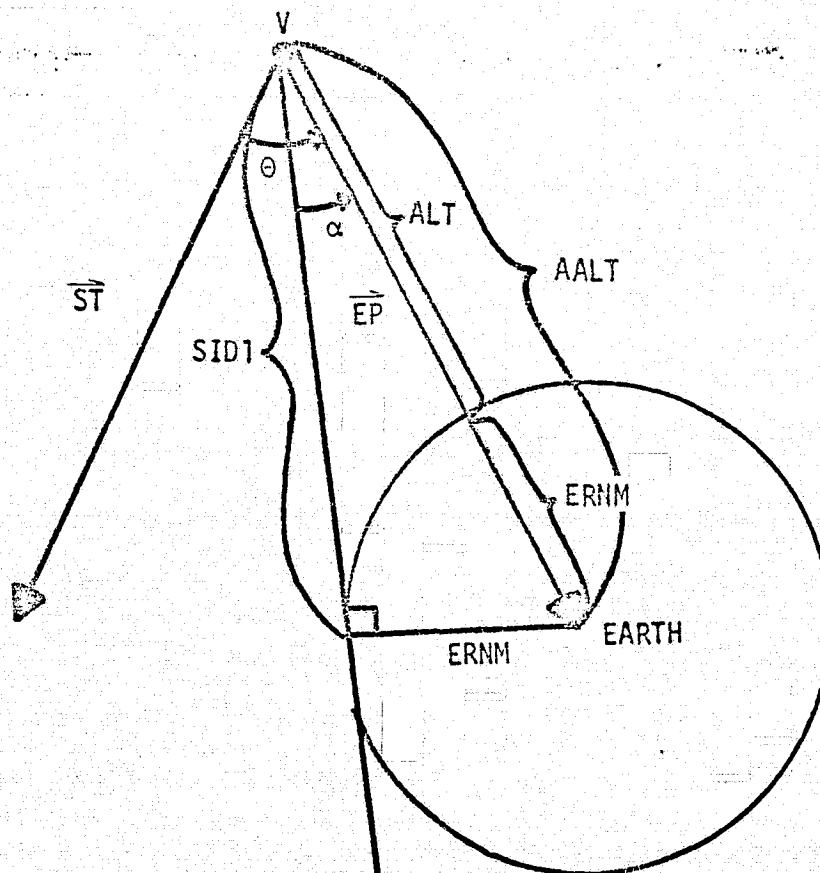


FIGURE 1: MODEL USED IN DETERMINING STAR TRACKER CONSTRAINT VIOLATION ANALYSIS LOGIC \*

\* All symbols used in model are defined in Appendix A.

The angle between the earth pointing vector in the body coordinate system (as defined in Reference (4)) and the line of sight to the horizon of the earth is computed using equation (1), where ERNM and SID1 are defined in Appendix A.

$$\alpha = \arctan \frac{ERNM}{SID1} \dots \dots \dots (1)$$

For purposes of testing earth pointing constraint violations,  $\alpha$  is computed irrespective of lighting conditions of the earth, a consideration that will be given to a later, more sophisticated model.

The angle for the testing of sun pointing constraint violations was set to a constant  $30^\circ$ , hence no  $\alpha$  computations are required. Expressions to compute theta ( $\theta$ ), the angle between the earth pointing or sun pointing vectors in the body coordinates, are given by equation (2) for earth pointing and equation (3) for sun pointing.

$$\theta = \arccos \left[ \frac{\vec{ST} \cdot \vec{EP}}{|\vec{ST}| |\vec{EP}|} \right] \dots \dots \dots (2)$$

$$\theta = \arccos \left[ \frac{\vec{ST} \cdot \vec{SP}}{|\vec{ST}| |\vec{SP}|} \right] \dots \dots \dots (3)$$

All symbols used in computing  $\theta$  and  $\alpha$ , including  $\vec{ST}$ ,  $\vec{EP}$  and  $\vec{SP}$ , are defined in Appendix A, and the basic figure for determining the math model used in program modifications is illustrated in Figure (1).

The star tracker pointing vector,  $\vec{ST}$ , for star trackers 1, 2, and 3 are computed by taking the transpose of the Body to Star Tracker coordinate transformation matrices obtained from Reference (5) for

each Star Tracker, and post multiplying each by the unit vector along the Z coordinate axis  $\begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$ . The earth pointing and sun pointing vectors used in equations (2) and (3) are computed by SAPT subroutine TARVEC in the earth centered, Aries Mean of 1950, inertial coordinate system described in Reference (4). The vectors are then transformed into the body coordinate system by a call from SAPT to subroutine BPCR (Body Pointing Conversion Routine). Once computed, the dot products of the star tracker pointing vectors and Earth or Sun pointing unit vectors for all pertinent pointing vectors are computed by subroutine UNVEC. Completing all preliminary computations, equations (2) and (3) are employed to compute  $\theta$  for each star tracker. Coding of Program SAPT is presented in Appendix B with all modifications indicated by the word "NEW" on the right hand side of the page.

The operation of this logic will be briefly described. A value of 20 degrees is added to the computed  $\alpha$  for earth pointing in accordance with the constraints specified in Reference (5). Every  $\theta$  corresponding to the combinations of star trackers and earth and sun pointing vectors is then computed. Each  $\theta$  is compared against  $\alpha$  (+ 20 degrees) for the earth and  $\alpha$  (= 30 degrees) for the sun, testing for  $\theta < \alpha$  ( $\alpha + 20^\circ$  for the earth). If such tests are successful, i.e.  $\theta < \alpha$ , a special code as defined in Reference (6) is output through modifications to SAPT output logic, indicating which constraint had been violated — Earth Pointing or Sun Pointing Constraints — and which Star Trackers are in violation of that

particular constraint. If the event being processed is not a platform alinement, computations and tests are not considered, and most computation logic is skipped.

Modifications for star tracker constraint violations analysis were used in the checkout of platform alinements being considered for certain inertial hold attitudes defined in the Preliminary Baseline Reference Mission (BRM) 2, Sortie Option 1 Attitude and Pointing Time Lines. Results indicated that nearly 90% of the alinements were performed with constraint violations, as illustrated in Reference (6). Sortie Options 2 and 3 of BRM 2 as well as BRM 1 showed similar results. Sortie Option 2 of BRM 2 is illustrated in Appendix C which shows that 8 out of 9 platform alinements violate star tracker pointing constraints when holding the prior inertial attitude.

Since extensive violations occurred in the inertial attitude just prior to a platform alinement, a maneuver to the LVLH attitude at 0,0,0 was then assumed, just prior to each Platform Alinement, and checkout attitude and pointing time lines were generated. Results showed no violations occurring for any Sortie Option of Mission 2, but due to the relatively low altitude for Mission 1, platform alinements performed in the inertial hold mode at an initial LVLH attitude of 0,0,0 always violated the earth pointing constraint for star tracker 3. (Appendix (D))

In updating BRM 1 and 2 time lines, the same violations were assumed

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to hold since new trajectories indicated no change in altitude. Checkout results indicated this to be the case. For updates to BRM 1, therefore, a slight Roll of  $+5^\circ$  was employed to assume an LVLH attitude at 0,0,5, with checkout results indicating that the selected attitude was sufficient to prevent further violation of constraints. A study of results using Star Tracker constraint violation detection logic revealed that updated Preliminary BRM 1 and 2 could be generated with platform alignments in LVLH attitudes at 0,0,5 and 0,0,0 respectively without violating any Star Tracker constraints. Results of updated time line generation for BRM 1 and 2 are illustrated in References (1) and (2).

## 5.0 CONCLUSION

The analysis results presented in Appendices C and D of this note are typical of those performed on preliminary Baseline Reference Mission Attitude and Pointing Time Lines to insure that no star tracker near earth or near sun pointing constraints were violated during IMU platform alignments.

The documented description of Star Tracker constraint violation modifications to program SAPT and descriptions of results using these modifications, as presented in this note, initially provides an adequate source of information. Program SAPT can be used to efficiently detect Star Tracker constraint violations and employ possible methods to insure avoidance of these violations. It is planned to upgrade the model used to detect star tracker constraint violations to

include an ellipsoidal earth model, earth occultation, earth lighting, and vehicle attitude dispersions. Capabilities such as these, to analyse attitude profiles, will continue to be developed, and analyses utilizing these capabilities will be performed to refine attitude and pointing profiles based on known attitude and pointing related constraints.

#### 6.0 REFERENCES

1. SSEOS 1.4-MIB-16, "Preliminary Baseline Reference Mission 1 Attitude and Pointing Time Lines", McDonnell Douglas Technical Services Company, Inc., dated 17 January 1975.
2. SSOES 1.4-MIB-12, "Preliminary Baseline Reference Mission 2 Attitude and Pointing Time Lines", McDonnell Douglas Technical Services Company, Inc., dated 8 January 1975.
3. SSEOS Design Note No. 1.4-2-6, "Attitude and Pointing Simulation Requirements and Program Updates", dated 24 December 1974.
4. JSC-09084, NASA TM X-58153, "Coordinate Systems for the Space Shuttle Program", dated October 1974.
5. SSEOS Design Note No. 1.4-2-4, "Orbiter Star Tracker Orientations, Operational Requirements and Coordinate Transformations", dated 24 October 1974.
6. SSEOS TM-1.4-MIB-9, "Detection of Star Tracker Constraint Violations", dated 16 December 1974.

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APPENDIX A: LIST OF SYMBOLS USED IN STAR TRACKER  
CONSTRAINT VIOLATION LOGIC

- (1) V - Reference Vehicle
- (2) ALT - Vehicle Altitude in Nautical Miles Referenced from Surface of the Earth - Computed in Subroutine NADIR and Returned to Program SAPT
- (3) ERNM - Earth Radius Expressed in Nautical Miles - Placed into SAPT by use of the DATA Statement
- (4) AALT - Total Distance from the Center to the Earth to the Reference Vehicle in Nautical Miles -  
AALT = ALT + ERNM
- (5) SID1 - Distance from Reference Vehicle to Tangent of Line of Sight to Horizon and the Earth in Nautical Miles -  
$$SID1 = \sqrt{(AALT)^2 - (ERNM)^2}$$
- (6)  $\vec{EP}$  - Earth Pointing Vector Expressed in Body Coordinates
- (7)  $\vec{SP}$  - Sun Pointing Vector Expressed in Body Coordinates
- (8)  $\vec{ST}$  - Star Tracker Pointing Vectors for Star Trackers 1, 2, and 3, Expressed in Body Coordinates
- (9)  $\alpha$  - Angle Between Earth Pointing Vector and Line of Sight to the Horizon of the Earth Expressed in Degrees -  
 $\alpha = [\text{ARCTAN} (ERNM/SID1)] \times 57.29577951$
- (10)  $\theta$  - Angle Between Earth Pointing Vector or Sun Pointing Vector and Star Tracker Pointing Vectors for each Star Tracker, Expressed in Body Coordinates -  
$$\theta_1 = \left[ \text{ARCCOS} \left( \frac{\vec{ST} \cdot \vec{EP}}{|\vec{ST}| |\vec{EP}|} \right) \right] \times 57.29577951$$
  
$$\theta_2 = \left[ \text{ARCCOS} \left( \frac{\vec{ST} \cdot \vec{SP}}{|\vec{ST}| |\vec{SP}|} \right) \right] \times 57.29577951$$

CODING OF PROGRAM SAPT WITHOUT SUBROUTINES

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00100 1*   CDI      **** PROGRAM SAPT ****
00100 2*   CDI      THE SHUTTLE ATTITUDE AND POINTING TIMELINE PROCESSOR (SAPT) IS THE
00100 3*   CDI      BASIC ATTITUDE AND POINTING TIMELINE GENERATION PROGRAM FOR
00100 4*   CDI      SHUTTLE. SAPT CAN GENERATE ATTITUDE AND POINTING TIMELINE TABLES
00100 5*   CDI      FOR DOCUMENTATION AND AT THE SAME TIME ALSO GENERATE ATTITUDE
00100 6*   CDI      TAPES FOR SUBSYSTEM EVALUATIONS. THE BASIC INPUT IS IN THE FORM
00100 7*   CDI      OF ATTITUDE AND POINTING DESCRIPTOR CARDS DEFINING THE NAME OF
00100 8*   CDI      THE EVENT, THE EVENT TIME, AND DESCRIPTORS DEFINING THE ATTITUDE
00100 9*   CDI      AND POINTING REQUIREMENTS FOR THE EVENT. THE PROGRAM REQUIRES
00100 10*  CDI      A TRAJECTORY TAPE MOUNTED ON UNIT F, AN EPHEMERIS TAPE MOUNTED ON
00100 11*  CDI      UNIT K, AND A PCF TAPE INCLUDING SAPT. IF AN ATTITUDE TAPE IS ALSO
00100 12*  CDI      TO BE GENERATED, A SAVE TAPE MUST BE MOUNTED ON THE TAPE UNIT
00100 13*  CDI      DEFINED BY ITAPE. THE FIRST INPUT CARD AFTER THE XQT CARD MUST BE
00100 14*  CDI      A BASE CARD GIVING THE BASE DATE TO MEASURE G.E.T. FROM AND THE
00100 15*  CDI      TAPE UNIT AND PRINT INTERVAL IF A ATTITUDE TAPE IS TO BE GENERATED
00100 16*  CDI      THERE IS ALSO AN INPUT FLAG WHICH DEFINES A TAPE UNIT TO WRITE A
00100 17*  CDI      DESCRIPTOR TIMELINE. AFTER THE BASE CARD, THE ATTITUDE AND POINT-
00100 18*  CDI      ING DESCRIPTOR CARDS FOLLOW. THERE MAY BE UP TO 4 CARDS REQUIRED
00100 19*  CDI      TO DEFINE EACH EVENT. THE FIRST CARD IN EACH EVENT SET IS THE
00100 20*  CDI      EVENT NAME CARD. UP TO 4 LINES OF EVENT DESCRIPTION CAN BE DEFINED
00100 21*  CDI      WITH 18 CHARACTERS TO EACH LINE. THE NEXT CARD IS THE ATTITUDE
00100 22*  CDI      REQUIREMENTS CARD GIVING THE EVENT TIME AND ATTITUDE ONLY REQUIR-
00100 23*  CDI      MENTS. IF THERE ARE NO POINTING REQUIREMENTS, THIS IS THE LAST
00100 24*  CDI      CARD OF THE SET. IF THERE ARE POINTING REQUIREMENTS, 1 OR 2 MORE

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00100 25. CD1 CARDS ARE REQUIRED DEPENDING ON THE NUMBER OF POINTING REQUIRE-
00100 26. CD1 MENTS. EVENT SETS SHOULD BE STACKED IN CHRONOLOGICAL ORDER, THE
00100 27. CD1 LAST CARD OF THE DECK IS LABELED 'END CARD' STARTING IN CC 1.
00100 28. CD1 THE INPUT PARAMETER DEFINITIONS FOR THE BASE CARD ARE GIVEN BELOW.
00100 29. CD1 THE INPUT DEFINITIONS FOR THE EVENT SETS ARE GIVEN IN SUBROUTINE
00100 30. CD1 'CARDIN'
00100 31. CD2 BASE CARD DEFINITIONS -
00100 32. CD2 NBASYR,NBASMT,NBASDV,NBASHR,NBASMN,BASSEC
00100 33. CD2 - BASE G.M.T. THAT G.E.T. IS MEASURED FROM (NOMINALLY THE
00100 34. CD2 LAUNCH G.M.T.
00100 35. CD2 ITAPE - UNIT ON WHICH THE COMMON FORMAT ATTITUDE TAPE IS TO BE
00100 36. CD2 WRITTEN. IF ZERO, NO TAPE IS REQUIRED.
00100 37. CD2 GHTINT - TIME INCREMENT BETWEEN PRINT POINTS DESIRED FOR THE
00100 38. CD2 COMMON FORMAT TAPE. (MINUTES)
00100 39. CD2 IUREAD - UNIT ON WHICH THE INPUT ATTITUDE DESCRIPTOR FILE WILL BE
00100 40. CD2 MOUNTED. IF ZERO, ALL INPUT WILL BE MANUAL.
00100 41. CD2 IUWRT - UNIT ON WHICH THE REVISED ATTITUDE DESCRIPTOR FILE IS TO
00100 42. CD2 BE WRITTEN. IF ZERO, NO TAPE IS TO BE WRITTEN.
00100 43. CD2 IHRST,MINST,SECS
00100 44. CD2 - GET TO START ATTITUDE TIMELINE IF A DESCRIPTOR FILE HAS
00100 45. CD2 BEEN PROVIDED. IF NOT INPUT, THE START OF THE DESCRIPTOR
00100 46. CD2 FILE, OR THE FIRST MANUAL INPUT, WHICHEVER IS EARLIER,
00100 47. CD2 WILL BE USED.
00100 48. CD2 IHNEND,MINEND,SECS
00100 49. CD2 - GET TO END ATTITUDE TIMELINE IF A DESCRIPTOR FILE HAS
00100 50. CD2 BEEN PROVIDED. IF NOT INPUT, THE END OF THE DESCRIPTOR
00100 51. CD2 FILE, OR THE LAST MANUAL INPUT, WHICHEVER IS LATER,
00100 52. CD2 WILL BE USED.
00100 53. C
00101 54. INTEGER ATTSYS,ALIGN
00103 55. REAL IANG1,IANG2,IANG12,IANG22
00104 56. DOUBLE PRECISION BASEJD,BASTIH,TGET,GHT,GHTP
00105 57. DOUBLE PRECISION GHTNXT,TSMCAL,TNEXT,TINTAP
00106 58. DOUBLE PRECISION XIHUDP,YIHUDP,ZIHUDP,RKHDP(3),VKHDP(3),GV(3)
00107 59. DOUBLE PRECISION GET
00110 60. DOUBLE PRECISION RSUNDP(3)
00111 61. REAL LIFTKG,ISPSEC
00112 62. REAL KX,KY,KZ,NUZ,MINTIM
00113 63. DIMENSION DUMMAT(15),R(3),V(3),RSUN(3),VSUN(3),RMOON(3),VMOON(3)
00114 64. DIMENSION TARGET(3),TDVEC(3),ATTLV(3,3),ATTI(3,3),SUNVEC(3),
00114 65. • PB(3),COEVEC(3),ATTECI(3,3)
00115 66. DIMENSION RKM(3),VKM(3),RKHU(3),RSUNU(3)
00116 67. DIMENSION ATTSR(3,3)
00117 68. DIMENSION SPARE(14),RSUNKH(3)
00120 69. DIMENSION ST12(3),ST3(3),SOSO(3),HOMO(3)
00121 70. DIMENSION SHAG1(3),SHAG2(3),SHAG3(3),SHAG4(3)
00122 71. COMMON/BASDT/ BASEJD,BASTIH,NBASYS,NBASMT,NBASDV,NBASHR,NBASMN,
00122 72. • BASSEC
00123 73. COMMON/ATPCOM/ GHTP,ATTP(3,3)
00124 74. COMMON/IERKCH/ IERR
00125 75. COMMON / VEHLE / KX,KY,KZ,NUZ,BETA,RASUN,DECSUN,RAMOON,DECHON
00126 76. COMMON/SHCALL/ TSMCAL,RSUN,VSUN,RMOON,VMOON
00127 77. COMMON/CARDS/IHR,MN,SECS,ATTSYS,IHNUM,IHVS,ANG1,ANG2,ANG3,
00127 78. • IHOLD,XRATE,YRATE,ZRATE,IPFLG,ALIGN,INSTID,IANG1,IANG2,
00127 79. • IYPE1,IDEF1,VAR1,VAR2,VAR3,ITARG1,VAR4,IDIN2,IANG12,IANG22,
00127 80. • IYPE2,IDEF2,VAR12,VAR22,VAR32,ITANG2,VAR42
00130 81. COMMON/TVCOM/ ITARG,ALPHAT,BETAT,WVEC(3),ALPHAC,BETAC,AT,
00130 82. • TLON,TLAT,IYPE,IDEF

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00257 141. 120 CONTINUE
00260 142. JPCARD = 1
00261 143. TGET = IHR + MN/60 + SECS/3600
00262 144. GMT = TGET + BASTIM
00263 145. 150 CONTINUE
00264 146. CALL TIMEC(GMT, IDAYN, IHRN, MINN, SECN)
00265 147. TIMTAP = GMT - BASTIM
00266 148. CALL TIMEC(TIMTAP, IDT, IHT, IMT, ST)
00267 149. IHT = IDT*24 + IHT
00270 150. TTAPE = SNGL(TIMTAP)
00271 151. IF(IHRN .GT. 21 .AND. (IDAYN - IDCALL) .EQ. 1) IDCALL = IDCALL-1
00273 152. IF((IDAYN - IDCALL) .GE. 0 .AND. (IDAYN - IDCALL) .LT. 2) GO TO 200
00275 153. IDCALL = IDAYN
00276 154. IF(IHRN .LT. 2) IDCALL = IDAYN - 1
00300 155. CALL INITIAL(IDCALL, ISTOP)
00301 156. IF(IISTOP .GT. 0) STOP
00303 157. 200 CONTINUE
00304 158. IF(IALIGN .NE. 1) GO TO 220
00306 159. CALL CRDFIL(2)
00307 160. CALL ATTDEF(GMT, ATTP)
00310 161. GMT = GMT
00311 162. CALL CRDFIL(1)
00312 163. 220 CONTINUE
00313 164. IF (ATTSYS .EQ. NBLANK) IBLANK = 1
00315 165. IF(ATTSYS .EQ. NBLANK) CALL CRDFIL(2)
00317 166. CALL ATTDEF(GMT, ATTECI)
00320 167. CALL CRDFIL(1)
00321 168. IF(ATTSYS .NE. NBLANK) GO TO 225
00323 169. DO 223 I=1,3
00326 170. DO 223 J=1,3
00331 171. ATTI(I,J) = ATTECI(I,J)
00332 172. 223 CONTINUE
00335 173. CALL EULER(ATTI, IVMS, ANG1, ANG2, ANG3, ATTECI)
00336 174. 225 CONTINUE
00337 175. CALL NADIR(GMT, SCLON, GDLAT, ALT)
00337 176. C
00337 177. C-----COMPUTE ANGLE ALPHA(ANGLE BETWEEN VEHICLE TO COE VECTOR AND
00337 178. C STAR TRACKER POINTING VECTOR) FOR EARTH POINTING CONSTRAINTS,
00337 179. C AND ADD 20 DEGREES TO ALPHA TO COMPUTE FINAL ALPHA FOR
00337 180. C STAR TRACKER EARTH POINTING CONSTRAINT VIOLATIONS CHECKOUT-----
00337 181. C
00340 182. AALT=ERNM*ALT
00341 183. TRIA1=(AALT**2)-(ERNM**2)
00342 184. SID1=SQRT(TRIA1)
00343 185. EALPHA=ATAN2(ERNM, SID1)
00344 186. EALPHA=EALPHA*RTD
00345 187. EALPHA=EALPHA+20.0
00346 188. WRITE(6,137)EALPHA
00351 189. 137 FORMAT(1X,F10.5)
00352 190. IF(IPTFLG .EQ. 0) GO TO 250
00354 191. CALL FILTVC(1)
00355 192. IF(ATTSYS.EQ.NBLANK) CALL CRDFIL(2)
00357 193. CALL TARVEC(GMT, NEWVEL, TARGET, TDOEC)
00360 194. CALL BPCR(1, ATTECI, TARGET, PB)
00361 195. CALL YNPTCH(2, YAWTAR, PTCTAR, PB)
00362 196. 250 CONTINUE
00363 197. ITYPE = 1
00364 198. IDEF = 8

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00365 199* CALL TARVEC(GMT,NEWVEL,SUNVEC,TDVEC)
00366 200* CALL BPCR(1,ATTECI,SUNVEC,PB)
00366 201* C
00366 202* C-----SAVE SUN POINTING VECTOR IN BODY COORDINATES-----
00366 203* C
00367 204* DO19I=1,3
00372 205* SO50(1)=PB(1)
00373 206* 19 CONTINUE
00375 207* CALL YWPTCH(2,YAWSUN,PTCSUN,PB)
00376 208* ITYPE = 1
00377 209* IDEF = 1
00400 210* CALL TARVEC(GMT,NEWVEL,COEVEC,TDVEC)
00401 211* CALL BPCR(1,ATTECI,COEVEC,PB)
00401 212* C
00401 213* C-----SAVE EARTH POINTING VECTOR IN BODY COORDINATES FOR LATER USE-----
00401 214* C
00402 215* DO13J=1,3
00405 216* HMO(J)=PB(J)
00406 217* 13 CONTINUE
00410 218* CALL YWPTCH(2,YAWCOE,PTCCOE,PB)
00411 219* CALL ACPI(1,2,2,4,1,3,3,IMUNUM,IMUNUM,GMT,GMT,ATTECI,TDVEC,
00411 220* • OMG,0.0,0.0,0.0,0.0,YRATE,ZRATE,XRATE,ATTLV,YOFF,ZOFF,XOFF)
00412 221* ZLVLH = ZOFF*RTD
00413 222* YLVLH = YOFF*RTD
00414 223* XLVLH = XOFF*RTD
00415 224* IF(ZLVLH.LT. -0.05) ZLVLH = 360.0 + ZLVLH
00417 225* IF(YLVLH.LT. -0.05) YLVLH = 360.0 + YLVLH
00421 226* IF(XLVLH.LT. -0.05) XLVLH = 360.0 + XLVLH
00423 227* IF(IHOLD.NE. 1) GO TO 260
00425 228* CALL ZLVDOT(7,XLVLH,YLVLH,ZLVLH,XRATE,YRATE,ZRATE)
00426 229* XRATE = XRATE*(SECPHR/RTD)
00427 230* YRATE = YRATE*(SECPHR/RTD)
00430 231* ZRATE = ZRATE*(SECPHR/RTD)
00431 232* 260 CONTINUE
00432 233* IF(IMUNUM.EQ. 0) IMUNUM=1
00434 234* M=3
00435 235* IF(IASTP.EQ.1) M=2
00437 236* CALL ACPI(1,2,2,4,3,3,M,IMUNUM,IMUNUM,GMT,GMT,ATTECI,TDVEC,
00437 237* • OMG,0.0,0.0,0.0,0.0,YRATE,ZRATE,XRATE,ATTI,YOFF,ZOFF,XOFF)
00440 238* ZIMU = ZOFF*RTD
00441 239* YIMU = YOFF*RTD
00442 240* XIMU = XOFF*RTD
00443 241* IF(ZIMU.LT. -0.05) ZIMU = 360.0 + ZIMU
00445 242* IF(YIMU.LT. -0.05) YIMU = 360.0 + YIMU
00447 243* IF(XIMU.LT. -0.05) XIMU = 360.0 + XIMU
00451 244* YAWTAR = YAWTAR*RTD
00452 245* PTCTAR = PTCTAR*RTD
00453 246* YAWSUN = YAWSUN*RTD
00454 247* PTCSUN = PTCSUN*RTD
00455 248* YAWCOE = YAWCOE*RTD
00456 249* PTCCOE = PTCCOE*RTD
00457 250* IF(SCLON.GT. 180.0) SCLON = SCLON - 360.0
00461 251* NUMCOM = 1
00462 252* DO 280 I=2,4
00465 253* DO 280 J=1,3
00470 254* IJ = (I-1)*3 + J
00471 255* IF(NEVENT(IJ).NE. NBLANK) NUMCOM = I
00473 256* 280 CONTINUE

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APPENDIX B  
Page 5 of 10

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00476 257. CALL TRAJC1 (GMT,R,V,JERR)
00477 258. IF (JERR .GT. 0) STOP
00501 259. RMAG = VECMG(R)
00502 260. IF (ITAPE .EQ. 0) GO TO 288
00504 261. RECFLG = 1.0
00504 262. C RECFLG- LAST RECORD IN FILE FLAG, IF LESS THAN 0.0 THIS IMPLIES
00504 263. C LAST RECORD IN FILE
00504 264. C PRFLG- FLAG INDICATING TYPE OF PRINT POINT
00505 265. CALL GMTCL (GMT,INBASYR,YEAR,GMONTH,GDAY,GHR,GMIN,GSEC )
00505 266. C SUBROUTINE GMTCL WILL COMPUTE GREENWICH MEAN TIME IN YEAR:
00505 267. C MONTH,DAY,HOURL,MINUTES, AND SECONDS FROM THE BEGINNING OF THE
00505 268. C BASE YEAR (INBASYR).
00506 269. GET = GMT - BASTIM
00506 270. C GET = TIME IN HOURS FROM LAUNCH
00507 271. DO 281 J=1,3
00512 272. RKM(J) = R(J) * 6378.16
00512 273. C RKM = VEHICLE RADIUS VECTOR (ECI) IN KM
00513 274. VKM(J) = V(J) * (6378.16 / 3600.0 )
00513 275. C VKM = VEHICLE VELOCITY VECTOR (ECI) IN KM/SEC
00514 276. RSUNDP(J) = DBLE(RSUN(J)) * 6378.16000
00515 277. RSUNKM(J) = SNGL(RSUNDP(J) )
00515 278. C RSUNKM = SUN VECTOR IN KM (ECI)
00516 279. 281 CONTINUE
00520 280. DO 285 I=1,3
00523 281. RKMDP(I) = DBLE (RKM(I) )
00523 282. C RKMDP = VEHICLE RADIUS VECTOR (DOUBLE PRECISION )
00524 283. VKMDP(I) = DBLE (VKM(I) )
00524 284. C VKMDP = VEHICLE VELOCITY VECTOR (DOUBLE PRECISION)
00525 285. 285 CONTINUE
00527 286. XIMUDP = DBLE (XIMU) / 57.295779500
00530 287. YIMUDP = DBLE (YIMU) / 57.295779500
00531 288. ZIMUDP = DBLE (ZIMU) / 57.295779500
00531 289. C YIMUDP,ZIMUDP,XIMUDP= PITCH, YAW, AND ROLL GIMBAL ANGLES (RADIAN)
00531 290. C WITH RESPECT TO INPUT REFMMAT
00532 291. RMAGKM = VECMG (RKM)
00532 292. C RMAGKM = VEHICLE GEOCENTRIC RADIUS (KM)
00533 293. CALL UNVEC (RKM,RKMU)
00533 294. C RKMU = VEHICLE UNIT RADIUS VECTOR (ECI)
00534 295. DECGCN = ASIN (RKMU(3))
00534 296. C DECGCN = VEHICLE GEOCENTRIC DECLINATION (RADIAN)
00534 297. RASGCN = ATAN2 (RKMU(2),RKMU(1) )
00535 298. C RASGCN = VEHICLE GEOCENTRIC RIGHT ASCENSION (RADIAN)
00536 299. VMAGKM = VECMG(VKM)
00536 300. C VMAGKM = VEHICLE INERTIAL VELOCITY VECTOR MAGNITUDE (KM/SEC)
00537 301. VALTKM = ALT * (6378.16 / 3443.9308855)
00537 302. C VALTKM = VEHICLE ALTITUDE ABOVE OBLATE EARTH (KM)
00540 303. VEHGDL = GDLAT / RTD
00540 304. C VEHGDL = VEHICLE GEODETIC LATITUDE (RADIAN)
00541 305. VEHLON = SCLON / RTD
00541 306. C VEHLON = VEHICLE LONGITUDE (RADIAN)
00542 307. CALL FPAZ (GMT,GAM1,PSI1,VELREL,GAMREL,PSIREL,GRAS )
00542 308. C GAM1 = INERTIAL FLIGHT PATH ANGLE (RADIAN)
00542 309. C PSI1 = INERTIAL AZIMUTH (RADIAN)
00542 310. C VELREL = RELATIVE VELOCITY VECTOR MAGNITUDE (KM/SEC)
00542 311. C GAMREL = RELATIVE FLIGHT PATH ANGLE (RADIAN)
00542 312. C PSIREL = RELATIVE AZIMUTH (RADIAN)
00542 313. C GRAS = RIGHT ASCENSION OF GREENWICH (RADIAN)
00543 314. AKM = A * ( 1.0 / 3280.833 )

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00720 373• IF(INUMLIN + NUMCOM) ,LE. MAXLIN) GO TO 300
00722 374• WRITE(6,950)
00724 375• 950 FORMAT(1H1,43X,'SHUTTLE ATTITUDE AND POINTING TIME LINE'//
00724 376• • 90X,'LOOK ANGLES LOOK ANGLES LOOK ANGLES'//
00724 377• • 34X,'VEHICLE POSITION LVLH ATTITUDE',7X,'ECI ATTITUDE',6X,
00724 378• • 1TO SUN',6X,'TO EARTH',8X,'TO TARGET'/5X,'GET',
00724 379• • 25X,'ALT',3X,'LAT',4X,'LON',4X,'YAW PITCH ROLL YAW PITCH ',
00724 380• • 'ROLL YAW PITCH YAW PITCH TARG YAW PITCH'//
00724 381• • 1X,'HRS MN SECS',7X,'EVENT',9X,'N MI DEG',4X,'DEG DEG DEG',
00724 382• • 3X,'DEG DEG DEG DEG DEG DEG DEG DEG ID',
00724 383• • 3X,'DEG DEG')
00725 384• NUMLIN = 7
00726 385• 300 CONTINUE
00726 386• C THE ATTITUDE AND POINTING TABLE IS WRITTEN BELOW,
00726 387• C
00726 388• C
00726 389• C-----COMPUTE ANGLE THETA BETWEEN STAR TRACKER POINTING VECTORS FOR
00726 390• C STAR TRACKERS 1,2, AND 3
00726 391• C AND SUN AND EARTH POINTING VECTORS, CHECK FOR EACH THETA
00726 392• C LESS THAN ALPHA=30 DEGREES FOR SUN, AND THETA LESS
00726 393• C THAN EARTH ALPHA + 20 DEG. FOR EARTH, AND OUTPUT
00726 394• C ANY VIOLATION ENCOUNTERED ACCORDING TO SPECIAL CODE
00726 395• C IF EVENT IS NOT PLATFORM ALINEMENT, THEN COMPUTATIONS
00726 396• C ARE NOT NECESSARY, AND LOGIC IS SKIPPED-----
00726 397• C
00727 398• IF(EVENT11;.NE.NAME) GO TO 3179
00731 399• CALL UNVEC(ST12,SMAG1)
00732 400• CALL UNVEC(ST3,SMAG2)
00733 401• CALL UNVEC(SO50,SMAG3)
00734 402• CALL UNVEC(HOMO,SMAG4)
00735 403• DOTP1=DOT(SMAG1,SMAG3)
00736 404• DOTP2=DOT(SMAG2,SMAG3)
00737 405• DOTP3=DOT(SMAG1,SMAG4)
00740 406• DOTP4=DOT(SMAG2,SMAG4)
00741 407• ATHET1=ACOS(DOTP1)
00742 408• ATHET1=ATHET1*RTD
00743 409• ATHET2=ACOS(DOTP2)
00744 410• ATHET2=ATHET2*RTD
00745 411• ATHET3=ACOS(DOTP3)
00746 412• ATHET3=ATHET3*RTD
00747 413• ATHET4=ACOS(DOTP4)
00750 414• ATHET4=ATHET4*RTD
00751 415• IZ=IQ
00752 416• IF(ATHET1.LT.SALPHA.AND.ATHET4.LT.EALPHA) GO TO 23
00754 417• IF(ATHET1.LT.SALPHA) IZ=IA
00756 418• IF(ATHET4.LT.EALPHA) IZ=IB
00760 419• GO TO 24
00761 420• 23 IZ=IH
00762 421• GO TO 28
00763 422• 24 IF(ATHET3.LT.EALPHA.AND.ATHET2.LT.SALPHA) GO TO 25
00765 423• IF(ATHET3.LT.EALPHA) IZ=IC
00767 424• IF(ATHET2.LT.SALPHA) IZ=ID
00771 425• GO TO 26
00772 426• 25 IZ=IG
00773 427• 26 IF(ATHET3.LT.EALPHA.AND.ATHET4.LT.EALPHA) GO TO 27
00775 428• GO TO 28
00776 429• 27 IZ=IE
00777 430• 28 CONTINUE

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01000 431. GO TO 9160
01001 432. 3179 IZ=10
01002 433. 9168 CONTINUE
01003 434. IF (JPCARD .EQ. 0) GO TO 305
01005 435. IF (ABS(ZLVLH).LT.0.0495) ZLVLH=.0
01007 436. IF (ABS(YLVLH).LT.0.0495) YLVLH=.0
01011 437. IF (ABS(XLVLH).LT.0.0495) XLVLH=.0
01013 438. IF (ABS(ZIMU).LT.0.0495) ZIMU=.0
01015 439. IF (ABS(YIMU).LT.0.0495) YIMU=.0
01017 440. IF (ABS(XIMU).LT.0.0495) XIMU=.0
01021 441. IF (ZLVLH.GT.359.9495) ZLVLH=.0
01023 442. IF (ZIMU.GT.359.9495) ZIMU=.0
01025 443. IF (IPTFLG .EQ. 0) WRITE(6,960) IHT,IMT,ST,(NEVENT(J),J=1,3),
01025 444. * ALT,GDLAT,SCLON,ZLVLH,YLVLH,XLVLH,ZIMU,YIMU,XIMU,YAWSUN,
01025 445. C
01025 446. C-----OUTPUT FORMATS ARE ALTERED TO ACCEPT SPECIAL
01025 447. C STAR TRACKER CONSTRAINT VIOLATION CODE-----
01025 448. C
01025 449. *PTCSUN,YAWCOE,PTCCOE,IZ
01055 450. 960 FORMAT(1X,13,1X,12,1X,F4.1,1X,3(A6),2(1X,F5.1),1X,F6.1,
01055 451. *2(1X,3(1X,F5.1)),2(1X,2(1X,F5.1))),1X,A1)
01056 452. IF (IPTFLG .NE. 0) WRITE(6,970) IHT,IMT,ST,(NEVENT(J),J=1,3),
01056 453. * ALT,GDLAT,SCLON,ZLVLH,YLVLH,XLVLH,ZIMU,YIMU,XIMU,YAWSUN,
01056 454. *PTCSUN,YAWCOE,PTCCOE,IZ,NAMTAR,YAWTAR,PTCTAR
01111 455. 970 FORMAT(1X,13,1X,12,1X,F4.1,1X,3(A6),2(1X,F5.1),1X,F6.1,
01111 456. *2(1X,3(1X,F5.1)),2(1X,2(1X,F5.1))),1X,A1,1X,A3,2(1X,F5.1))
01112 457. GO TO 306
01113 458. 305 CONTINUE
01114 459. IF (ABS(ZLVLH).LT.0.0495) ZLVLH=.0
01116 460. IF (ABS(YLVLH).LT.0.0495) YLVLH=.0
01120 461. IF (ABS(XLVLH).LT.0.0495) XLVLH=.0
01122 462. IF (ABS(ZIMU).LT.0.0495) ZIMU=.0
01124 463. IF (ABS(YIMU).LT.0.0495) YIMU=.0
01126 464. IF (ABS(XIMU).LT.0.0495) XIMU=.0
01130 465. IF (ZLVLH.GT.359.9495) ZLVLH=.0
01132 466. IF (ZIMU.GT.359.9495) ZIMU=.0
01134 467. IF (IPTFLG .EQ. 0) WRITE (6,960) IHT,IMT,ST,NCARD,NCARD,NCARD,
01134 468. *ALT,GDLAT,SCLON,ZLVLH,YLVLH,XLVLH,ZIMU,YIMU,XIMU,YAWSUN,
01134 469. *PTCSUN,YAWCOE,PTCCOE,IZ
01163 470. IF (IPTFLG .NE. 0) WRITE (6,970) IHT,IMT,ST,NCARD,NCARD,NCARD,
01163 471. *ALT,GDLAT,SCLON,ZLVLH,YLVLH,XLVLH,ZIMU,YIMU,XIMU,YAWSUN,
01163 472. *PTCSUN,YAWCOE,PTCCOE,IZ,NAMTAR,YAWTAR,PTCTAR
01215 473. 306 CONTINUE
01216 474. IF (NUMCOM .EQ. 1) GO TO 350
01220 475. DO 320 J=2,NUMCOM
01223 476. IJ = (J-1)*3
01224 477. WRITE(6,980) NEVENT(IJ+1),NEVENT(IJ+2),NEVENT(IJ+3)
01231 478. 980 FORMAT(13X,3(A6))
01232 479. 320 CONTINUE
01232 480. C
01234 481. 350 CONTINUE
01235 482. GETWRT = IHR + MN/60.0 + SECS/3600.0
01235 483. C THE DESCRIPTOR TAPE IS WRITTEN BELOW.
01235 484. C
01236 485. IF (IUWRT .GT. 0) WRITE(IUWRT) GETWRT,ATTSYS,IMUNUM,IVMS,
01236 486. * ANG1,ANG2,ANG3,IHOLD,XRATE,YRATE,ZRATE,IPTFLG,ALIGN,INSTID,
01236 487. * IANG1,IANG2,ITYPE1,IDEF1,VAR1,VAR2,VAR3,ITARG1,VAR4,IDIN2,
01236 488. * IANG12,IANG22,ITYPE2,IDEF2,VAR12,VAR22,VAR32,ITARG2,VAR42,

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01236 489*      * (NEVENT(J),J=1,12),NAMTAR
01236 490*      C
01307 491*      NUMLIN = NUMLIN + NUMCOM
01310 492*      IF (GMTINT .GT. 1.E-4) GO TO 400
01312 493*      IF (IBLANK .NE. 1) CALL CRDFIL(3)
01314 494*      IBLANK = 0
01315 495*      IF (IERR .EQ. 0) GO TO 100
01317 496*      IF (IUWRT .GT. 0) ENDFILE IUWRT
01321 497*      STOP
01322 498*      400 CONTINUE
01323 499*      GMT = GMT + GMTINT/60.000
01324 500*      IF (JPCARD .EQ. 0) GO TO 450
01326 501*      CALL CRDFIL(1)
01327 502*      IF (ATTSYS .NE. NBLANK) CALL CRDFIL(3)
01327 503*      C THE CALL TO GETDES OBTAINS THE NEXT EVENT SET
01327 504*      C
01331 505*      CALL GETDES(IUREAD,ISTOP)
01331 506*      C
01332 507*      IF (ITAPE .GT. 0 .AND. IERR .LT. 0) RECFLG = - 1.0
01334 508*      IF (RECFLG .LT. 0) WRITE(ITAPE) RECFLG,PRTFLG,YEAR,GMONTH,GDAY,
01334 509*      *GHR,GMIN,GSEC,GET,(RKMDP(1),I=1,3),(VKMDP(1),I=1,3),(DV(1),I=1,3),
01334 510*      *YIMUDP,ZIMUDP,XIMUDP,RHAGKM,DECGCN,RASGCN,VMAGKM,GAM1,PS11,
01334 511*      *VALTKN,VEHGDL,VEHLON,VELREL,GAMREL,PSIREL,GRAS,REV,AKM,E,RADINC,
01334 512*      *ASCNR,ARGPR,TRUEAN,PERIOD,DYNPR,DRAGKG,LIFTKG,WGTKG,THRKG,ISPSEC,
01334 513*      *EGRAVC,SHADOW,(ATTECI(1,J),J=1,3),(ATTECI(2,J),J=1,3),
01334 514*      * (ATTECI(3,J),J=1,3),YLVHR,ZLVHR,XLVHR,ALSR,BTSR,GMSR,PTSUNR,
01334 515*      *YWSUNR,PTCUER,YWCOER,(RSUNKH(1),I=1,3),(SPARE(1),I=1,14)
01462 516*      IF (RECFLG .LT. 0) ENDFILE ITAPE
01464 517*      IF (IERR .NE. 0) STOP
01466 518*      CALL CRDFIL(1)
01467 519*      JPCARD = 0
01470 520*      TNEXT = IHR + MN/60 + SECS/3600
01471 521*      GMTNXT = TNEXT + BASTIM
01472 522*      450 CONTINUE
01473 523*      IF ( (GMTNXT-GMT) .LE. 1.E-5 ) CALL CRDFIL(1)
01475 524*      IF ( (GMTNXT-GMT) .LE. 1.E-5 ) GO TO 120
01477 525*      ATTSYS = NBLANK
01500 526*      ALIGN = 0
01501 527*      IF (IERR .EQ. 0) GO TO 150
01503 528*      STOP
01504 529*      END

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END OF COMPILATION:  
SAPT CODE SYMBOLIC  
SAPT CODE RELOCATABLE

NO DIAGNOSTICS.

27 JUN 74	15:33:38	0	02621512	14	424	(DELETED)
27 JUN 74	15:33:38	1	01746122	84	1	(DELETED)
		0	01746246	14	157	

APPENDIX C: RESULTS OF STAR TRACKER CONSTRAINT VIOLATION  
ANALYSIS FOR SORTIE OPTION 2 OF BRM 2 WITH  
PLATFORM ALINEMENTS PERFORMED IN THE INERTIAL  
HOLD MODE AT THE INERTIAL ATTITUDE JUST PRIOR  
TO THE ALINEMENT \*

\* Included are printouts for Alpha ( $\alpha$ ) + 20° for earth pointing constraint violations, printed after each event; and angles Theta ( $\theta$ ) for Star Tracker 1 and 2 and the Sun, Star Tracker 3 and the Sun, Star Trackers 1 and 2 and the Earth, and Star Tracker 3 and the Earth, printed in a line of four numbers prior to each platform alinement.

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PRELIMINARY BRM MISSION 2 - OPTION 2  
SHUTTLE ATTITUDE AND POINTING TIME LINE  
WITH STAR TRACKER CONSTRAINTS INDICATED

APPENDIX C  
Page 1 of 8

GET HRS MN SECS	EVENT	VEHICLE POSITION			VLH ATTITUDE			ECI ATTITUDE			LOOK ANGLES TO SUN		LOOK ANGLES TO EARTH		LOOK ANGLES TO TARGET		
		ALT H MI	LAT DEG	LOX DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	YAW DEG	PITCH DEG	TARG ID	YAW DEG	PITCH DEG
50 00	HNVR TO INERTIAL HOLD ATT FOR EXP SETUP AND CHECKOUT	233.6	50.5	93.8	90.0	.0	.0	257.9	34.9	19.8	356.4	345.4	.0	270.0			
89.39802																	
51 00	TORS 41W	235.3	44.2	-21.4	89.8	.1	232.0	257.9	34.9	19.8	356.5	345.5	269.9	38.0			
89.39802																	
51 00	TORS 171W	235.3	44.2	-21.4	89.8	.1	232.0	257.9	34.9	19.8	356.5	345.5	269.9	38.0			
89.48655																	
53 00	BEGIN INERTIAL HOLD FOR SLEEP	233.2	-36.5	21.6	90.0	.0	.0	257.3	34.9	43.5	3.2	345.7	.0	270.0			
89.40141																	
55 00	BEGIN SLEEP PERIOD	235.2	-24.0	122.2	90.2	359.7	103.9	257.3	34.9	43.5	3.3	345.8	89.7	13.9			
89.50570																	
63 00	END SLEEP PERIOD	232.7	22.2	34.8	89.3	358.6	159.9	257.3	34.9	43.5	3.5	346.0	85.9	69.9			
89.48935																	
64 24	TORS 41W	233.1	-6.4	-7.5	90.3	358.2	124.7	257.3	34.9	43.5	3.5	346.1	67.8	34.7			
89.48935																	
64 24	TORS 171W	233.1	-6.4	-7.5	90.3	358.2	124.7	257.3	34.9	43.5	3.5	346.1	67.8	34.7			
89.51723																	
98.94534	102.96961 27.14784 116.39949																
64 30	PLATFORM ALINE	232.4	12.7	4.5	89.6	358.3	147.9	257.3	34.9	43.5	3.5	346.1	86.7	57.9			
89.32095																	
64 45	HNVR TO VLH ATT FOR NV-1 CAL	237.2	52.0	54.2	.0	.0	180.0	335.6	346.7	36.0	268.7	346.5	.0	90.0			
89.60740																	
65 15	BEGIN INERTIAL HOLD	230.3	-7.8	169.5	.0	.0	180.0	91.7	54.0	103.6	258.3	6.9	.0	90.0			
89.43381																	
65 55	HNVR TO VLH ATT FOR NV-1 CAL	234.4	-12.9	-35.3	.0	.0	180.0	226.9	307.8	111.0	245.4	358.8	.0	90.0			
89.33717																	
66 25	BEGIN INERTIAL HOLD	236.8	53.9	73.8	.0	.0	180.0	350.8	8.6	35.3	263.1	348.4	.0	90.0			
89.48037																	
67 00	HNVR TO VLH ATT FOR NV-1 OPS	233.3	-42.0	177.4	.0	.0	180.0	143.6	27.3	139.9	266.6	13.0	.0	90.0			
89.32314																	
67 50	BEGIN INERTIAL HOLD	237.1	50.1	1.0	.0	.0	180.0	332.3	343.2	36.7	270.4	346.6	.0	90.0			
89.52163																	
69 10	HNVR TO VLH ATT FOR NV-2 EARLY OPS	232.3	15.2	-64.7	.0	.0	180.0	285.1	309.0	65.2	260.7	352.2	.0	90.0			
89.36457																	
69 35	BEGIN INERTIAL HOLD	236.1	48.0	47.5	.0	.0	180.0	359.4	20.7	37.7	260.9	350.3	.0	90.0			
89.34317																	
71 45	HNVR TO VLH ATT FOR NV-1 AND EO-77R OPS	236.6	-53.5	135.0	.0	.0	180.0	157.1	9.5	144.6	270.9	13.1	.0	90.0			
89.39530																	
72 45	BEGIN INERTIAL	235.4	38.9	15.7	.0	.0	180.0	9.6	32.2	42.5	259.3	352.5	.0	90.0			

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HOLD																
89.50041	73 38	.0	MNVR TO LVLH ATT	232.8	-20.1	-158.4	-0.0	.0	180.0	214.9	311.7	120.7	282.8	2.5	.0	90.0
		FOR NV-1 OPS AND														
		EO-7/H OPS														
89.42680	74 25	.0	BEGIN INERTIAL	234.6	18.7	10.8	-0.0	.0	180.0	37.1	49.2	61.1	257.2	357.8	.0	90.0
HOLD																
89.32832	75 0	.0	MNVR TO LVLH ATT	237.0	-49.4	141.4	.0	-0.0	180.0	176.6	341.5	142.9	277.5	10.6	.0	90.0
		FOR NV-1 OPS														
89.37355	75 32	.0	TORS 41W	235.9	43.1	-132.0	179.9	56.3	359.9	176.6	341.5	142.9	277.5	10.6	180.0	326.3
89.37355	75 32	.0	TORS 171W	235.9	43.1	-132.0	179.9	56.3	359.9	176.6	341.5	142.9	277.5	10.6	180.0	326.3
89.30029	74.40482	19.71246	141.91470	76.86741												
89.39677	75 38	.0	PLATFORM ALINE	237.7	53.9	-102.1	179.9	33.1	-0.0	176.6	341.5	142.9	277.5	10.6	180.0	303.1 0
89.39677	75 53	.0	BEGIN INERTIAL	235.3	33.8	-25.6	-0.0	.0	180.0	15.1	37.4	46.0	258.9	353.4	.0	90.0
HOLD																
89.52421	76 23	.0	MNVR TO LVLH ATT	232.3	-1.8	142.7	-0.0	-0.0	180.0	249.0	304.9	92.8	282.7	358.5	.0	90.0
		FOR NV-1 OPS														
89.31220	78 50	.0	MNVR TO INERTIAL	237.4	53.4	-112.2	90.0	.0	.0	252.4	34.9	167.6	4.6	11.9	.0	270.0
		HOLD ATT FOR SLEEP														
89.39900																

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## SHUTTLE ATTITUDE AND POINTING TIME LINE

GET HRS MN SECS	EVENT	VEHICLE POSITION			LVLH ATTITUDE			ECI ATTITUDE			LOOK ANGLES TO SUN		LOOK ANGLES TO EARTH		LOOK ANGLES TO TARGET		
		ALT N MI	LAT DEG	LONG DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	YAW DEG	PITCH DEG	TARG ID	YAW DEG	PITCH DEG
79 00	.0 BEGIN SLEEP PERIOD	235.3	-31.3	-70.4	90.0	.0	36.6	252.4	34.9	167.6	4.6	11.9	90.0	308.6			
89.58441																	
87 00	.0 END SLEEP PERIOD	230.8	-14.5	-156.9	90.3	1.2	94.6	252.4	34.9	167.6	4.3	12.0	91.2	4.6			
89.50941																	
86 39	.0 TDRS 41W	232.6	-32.5	-166.1	91.0	1.2	117.4	252.4	34.9	167.6	4.2	12.0	91.3	27.4			
89.50941																	
88 39	.0 TDRS 171W	232.6	-32.5	-166.1	91.0	1.2	117.4	252.4	34.9	167.6	4.2	12.0	91.3	27.4			
89.41213																	
73.01617	103.77608 34.37802 122.56078																
86 45	.0 PLATFORM ALINE	235.0	-47.6	-144.4	91.4	.7	140.6	252.4	34.9	167.6	4.2	12.0	91.1	50.6 C			
89.34898																	
89 00	.0 MNVR TO LVLH ATT FOR NV-1 CAL	236.5	-44.3	-60.3	.0	.0	180.0	180.4	334.1	140.5	276.5	10.8	.0	90.0			
89.46325																	
89 30	.0 BEGIN INERTIAL HOLD	233.7	44.2	17.1	.0	.0	180.0	320.9	334.3	39.4	277.1	349.6	.0	90.0			
89.47289																	
90 15	.0 MNVR TO LVLH ATT FOR NV-1 CAL	233.5	-40.4	179.6	.0	.0	180.0	136.4	30.1	138.6	261.8	9.6	.0	90.0			
89.53268																	
90 45	.0 BEGIN INERTIAL HOLD	232.1	-9.8	-51.2	.0	.0	180.0	230.3	306.5	106.2	282.2	3.2	.0	90.0			
89.32501																	
92 00	.0 MNVR TO LVLH ATT FOR NV-1 AND NV-2 EARTH OPS	237.1	-54.4	-139.2	.0	.0	180.0	164.8	353.1	144.8	270.9	12.6	.0	90.0			
89.57644																	
93 5	.0 INERTIAL HOLD	231.0	8.5	94.2	.0	.0	180.0	52.4	53.9	75.8	257.9	356.6	.0	90.0			
89.53321																	
93 50	.0 MNVR TO LVLH ATT FOR NV-2 EARTH OPS	232.0	-13.3	-100.8	.0	.0	180.0	222.9	307.9	111.6	281.7	4.8	.0	90.0			
89.40639																	
94 30	.0 BEGIN INERTIAL HOLD	235.1	33.1	51.6	.0	.0	180.0	12.4	38.0	46.5	261.5	350.6	.0	90.0			
89.52697																	
95 30	.0 MNVR TO LVLH ATT FOR NV-1 OPS	232.2	8.7	-110.6	.0	.0	180.0	267.7	306.3	74.9	282.6	359.4	.0	90.0			
89.56790																	
96 10	.0 BEGIN INERTIAL HOLD	231.2	12.1	44.6	.0	.0	180.0	44.8	52.6	70.2	258.3	355.1	.0	90.0			
89.44310																	
96 50	.0 MNVR TO LVLH ATT FOR EO-7/8 OPS	234.2	-31.9	-162.6	.0	.0	180.0	193.5	320.9	132.5	278.4	9.6	.0	90.0			
89.30536																	
97 20	.0 BEGIN INERTIAL HOLD	237.5	52.9	-78.0	.0	.0	180.0	331.0	348.8	35.7	275.1	348.4	.0	90.0			
89.39484																	
98 20	.0 MNVR TO LVLH ATT FOR NV-2 EARTH OPS AND EO-7/8 OPS	235.4	-40.3	164.1	.0	.0	180.0	183.1	329.3	138.4	276.0	11.3	.0	90.0			

89.34343

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98 55	.0 BEGIN INERTIAL HOLD	236.6	54.7	-89.9	-0.0	-0.0	180.0	335.1	354.9	35.0	273.9	347.8	0.0	90.0
89.51596														
99 30	.0 MNVR TO LVLH ATT FOR NV-1 OPS	232.5	-31.2	27.3	0.0	0.0	180.0	123.5	39.5	132.2	258.6	5.8	0.0	90.0
89.36811														
99 54	.0 TDORS 41W	236.0	-37.8	143.7	178.6	87.2	358.5	123.5	39.5	132.2	258.6	5.8	180.1	357.2
89.36811														
99 54	.0 TDORS 171W	236.0	-37.6	143.7	178.6	87.2	356.5	123.5	39.5	132.2	258.6	5.8	180.1	357.2
89.42457														
79.18516	1.84867 110.98168 71.44991													
100 0	.0 PLATFORM ALINE	234.7	-20.4	159.8	179.2	64.0	359.8	123.5	39.5	132.2	258.6	5.8	180.1	334.0 0
89.50235														
100 15	.0 BEGIN INERTIAL HOLD	232.8	26.7	-168.6	0.0	0.0	180.0	297.3	316.7	51.8	282.0	355.5	0.0	90.0
89.52514														
101 45	.0 MNVR TO LVLH ATT FOR NV-2 EARTH OPS	232.2	17.4	160.7	0.0	0.0	180.0	282.6	310.2	62.3	282.7	358.4	0.0	90.0
89.41299														
102 15	.0 MNVR TO INERTIAL HOLD FOR SLEEP	234.9	34.0	-67.4	90.0	0.0	0.0	248.0	34.9	132.5	7.1	10.8	0.0	270.0
89.36879														
103 0	.0 BEGIN SLEEP PERIOD	236.0	-38.7	96.0	90.1	359.9	174.0	248.0	34.9	132.5	7.0	10.8	89.2	84.0
89.53301														
111 0	.0 END SLEEP PERIOD	232.1	6.7	11.9	89.8	358.7	230.0	248.0	34.9	132.5	6.8	11.0	271.7	40.0
89.41853														
112 24	.0 TDORS 41W	234.8	-21.9	-30.3	90.7	358.6	194.7	248.0	34.9	132.5	6.7	11.1	275.5	75.2
89.41853														
112 24	.0 TDORS 171W	234.8	-21.9	-30.3	90.7	358.6	194.7	248.0	34.9	132.5	6.7	11.1	275.5	75.2
89.51991														

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SHUTTLE ATTITUDE AND POINTING TIME LINE

GET HRS MN SECS	EVENT	VEHICLE POSITION			LVLH ATTITUDE			ECI ATTITUDE			LOOK ANGLES TO SUN		LOOK ANGLES TO EARTH		LOOK ANGLES TO TARGET		
		ALT N MI	LAT DEG	LOX DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	YAW DEG	PITCH DEG	TARG ID	YAW DEG	PITCH DEG
73.93813	106.29785	32.98704	49.68026														
112 30	.0 PLATFORM ALINE	232.4	-3.1	-17.7	90.1	358.4	218.0	246.0	34.9	132.5	6.7	11.1	272.6	52.0	E		
89.33221																	
113 45	.0 MNVR TO LVLH ATT FOR NV-1 CAL	236.9	-52.0	-97.4	.0	.0	180.0	165.5	346.4	144.0	268.0	13.4	.0	90.0			
89.47314																	
114 15	.0 BEGIN INERTIAL HOLD	233.5	33.8	-14.6	.0	.0	180.0	304.0	322.9	45.8	283.0	356.0	.0	90.0			
89.54088																	
114 45	.0 MNVR TO LVLH ATT FOR NV-1 CAL	231.9	17.6	117.4	.0	.0	180.0	31.3	49.9	62.5	260.7	350.0	.0	90.0			
89.32237																	
115 15	.0 BEGIN INERTIAL HOLD	237.1	-55.0	-139.5	.0	.0	180.0	158.3	356.1	145.0	264.9	12.7	.0	90.0			
89.52450																	
115 35	.0 MNVR TO LVLH ATT FOR NV-1 OPS	232.3	-6.6	-67.2	.0	.0	180.0	231.9	305.6	101.1	281.3	7.7	.0	90.0			
89.43507																	
116 40	.0 BEGIN INERTIAL HOLD	234.4	-47.3	-149.8	.0	.0	180.0	139.4	-21.4	-142.1	-258.8	-8.1	.0	90.0			
89.55260																	
118 45	.0 MNVR TO LVLH ATT FOR NV-2 EARTH OPS AND EO-7/8 OPS	231.6	5.7	-106.8	.0	.0	180.0	257.3	305.5	79.8	283.0	5.2	.0	90.0			
89.46132																	
119 25	.0 BEGIN INERTIAL HOLD	233.8	15.0	48.3	.0	.0	180.0	34.9	51.3	65.9	260.5	349.6	.0	90.0			
89.55415																	
120 15	.0 MNVR TO LVLH ATT FOR NV-1 OPS AND NV-2 OPS	231.5	-4.1	-136.5	.0	.0	180.0	236.4	305.1	96.7	281.6	8.1	.0	90.0			
89.55463																	
121 0	.0 BEGIN INERTIAL HOLD	231.5	8.9	28.7	.0	.0	180.0	46.2	53.8	75.1	259.3	350.6	.0	90.0			
89.52998																	
121 45	.0 MNVR TO LVLH ATT FOR EO-7/8 OPS	232.1	-13.8	-166.3	.0	.0	180.0	216.8	308.1	112.2	279.6	10.6	.0	90.0			
89.31809																	
122 12	.0 BEGIN INERTIAL HOLD	237.2	55.2	-77.4	.0	.0	180.0	333.0	358.3	34.9	278.1	348.2	.0	90.0			
89.43719																	
122 50	.0 MNVR TO LVLH ATT FOR NV-1 OPS	234.4	-42.1	46.0	.0	.0	180.0	132.2	28.2	139.6	256.7	5.4	.0	90.0			
89.29574																	
123 45	.0 BEGIN INERTIAL HOLD	237.8	55.1	-101.4	.0	.0	180.0	332.6	358.1	34.9	278.5	348.3	.0	90.0			
89.36388																	
124 39	.0 TDRS 41W	236.4	-47.5	110.2	180.2	331.2	359.9	332.6	358.1	34.9	278.6	348.3	359.9	298.8			
89.35388																	
124 39	.0 TDRS 171W	236.4	-47.5	110.2	180.2	331.2	359.9	332.6	358.1	34.9	278.6	348.3	359.9	298.8			
89.42774																	

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96.70908	21.17232	122.98055	96.65373														
124 45	.0	PLATFORM ALIVE	234.6	-32.3	131.8	180.3	308.0	359.8	332.6	358.1	34.9	278.6	348.3	359.8	322.0	0	
89.52720																	
125 0	.0	MMVR TO LVLH ATT FOR NV-1 OPS AND NV-2 EARTH OPS	232.2	14.4	164.3	-0.0	0.0	180.0	273.0	308.6	64.3	284.0	4.1	0.0	90.0		
89.41005																	
125 30	.0	MMVR TO INERTIAL ATT FOR SLEEP	235.0	36.6	-64.7	90.0	0.0	0.0	243.6	34.8	136.2	2.4	14.4	0.0	270.0		
89.37492																	
127 0	.0	BEGIN SLEEP PERIOD	235.9	44.4	-99.3	89.8	0.1	348.0	243.6	34.8	136.2	2.3	14.5	209.4	282.0		
89.57663																	
135 0	.0	END SLEEP PERIOD	231.0	1.2	-179.1	89.9	1.5	44.0	243.6	34.8	136.2	2.0	14.7	92.1	314.0		
89.39850																	
136 24	.0	TDRS 41W	235.3	29.4	137.4	89.0	1.3	8.7	243.6	34.8	136.2	2.0	14.7	90.8	278.8		
89.39850																	
136 24	.0	TDRS 171W	235.3	29.4	137.4	89.0	1.3	8.7	243.6	34.8	136.2	2.0	14.7	90.8	278.8		
89.53533																	
70.30524	101.40363	143.00717	115.23689														
136 30	.0	PLATFORM ALIVE	232.0	10.9	151.2	89.6	1.6	32.0	243.6	34.8	136.2	2.0	14.7	93.1	302.0		
89.49382																	
136 45	.0	MMVR TO LVLH ATT FOR NV-1 CAL	233.0	-35.4	-175.3	0.0	0.0	180.0	121.7	35.5	135.4	254.1	0.7	0.0	90.0		
89.29719																	
137 45	.0	BEGIN INERTIAL HOLD	237.7	54.6	61.7	-0.0	-0.0	180.0	335.3	5.8	35.1	279.6	347.1	0.0	90.0		
89.39832																	

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## SHUTTLE ATTITUDE AND POINTING TIME LINE

GET HRS MN SECS	EVENT	VEHICLE POSITION			LVLH ATTITUDE			ECI ATTITUDE			LOOK ANGLES TO SUN		LOOK ANGLES TO EARTH		LOOK ANGLES TO TARGET		
		ALT	LAT	LOH	YAW	PITCH	ROLL	YAW	PITCH	ROLL	YAW	PITCH	YAW	PITCH	TARG	YAW	PITCH
		H MI	DEG	DEG	DEG	DEG	DEG	DEG	DEG	DEG	DEG	DEG	DEG	DEG	ID	DEG	DEG
139 12	.0 MNVR TO LVLH ATT FOR NV-2 EARTH OPS	236.3	51.9	2	.0	.0	180.0	321.5	346.6	36.0	284.2	352.0	.0	90.0			
89.58815																	
139 40	.0 BEGIN INERTIAL HOLD	230.7	-1.4	111.6	.0	.0	180.0	64.3	55.1	92.8	257.8	349.1	.0	90.0			
89.36613																	
140 10	.0 MNVR TO LVLH ATT FOR NV-1 OPS	236.3	-46.7	124.4	.0	.0	180.0	167.7	337.3	141.8	265.2	15.7	.0	90.0			
89.49162																	
140 36	.0 BEGIN INERTIAL HOLD	233.0	30.7	-59.2	.0	.0	180.0	295.1	320.1	40.1	286.3	1.8	.0	90.0			
89.38033																	
141 48	.0 MNVR TO LVLH ATT FOR NV-1 OPS AND EO-7/8 OPS	235.7	-34.3	130.1	.0	.0	180.0	182.0	323.1	134.4	270.4	16.6	.0	90.0			
89.49988																	
142 38	.0 BEGIN INERTIAL HOLD	232.8	24.1	47.3	.0	.0	180.0	15.6	45.6	54.7	265.7	343.8	.0	90.0			
89.50961																	
143 40	.0 MNVR TO LVLH ATT FOR NV-2 EARTH OPS	232.6	24.4	-111.9	.0	.0	180.0	285.9	314.9	54.0	286.2	4.7	.0	90.0			
89.40041																	
144 6	.0 BEGIN INERTIAL HOLD	235.2	38.6	9.4	.0	.0	180.0	356.4	32.5	42.6	271.9	343.2	.0	90.0			
89.46377																	
145 0	.0 MNVR TO LVLH ATT FOR NV-1 OPS AND EO-7/8 OPS	233.7	-16.7	-162.6	.0	.0	180.0	207.1	309.6	116.4	276.6	15.7	.0	90.0			
89.36439																	
145 25	.0 BEGIN INERTIAL HOLD	236.1	52.9	-90.0	.0	.0	180.0	322.0	348.9	35.6	285.1	351.9	.0	90.0			
89.49424																	
146 6	.0 MNVR TO LVLH ATT FOR NV-1 OPS AND EO-7/8 OPS	233.0	-42.3	51.9	.0	.0	180.0	128.0	28.0	139.7	253.0	2.1	.0	90.0			
89.32298																	
147 6	.0 BEGIN INERTIAL HOLD	237.1	51.8	-64.5	.0	.0	180.0	339.5	14.0	36.1	279.2	345.3	.0	90.0			
89.33117																	
147 51	.0 TDRS 41W	236.9	-53.7	94.9	180.1	6.0	.0	339.5	14.0	36.1	279.3	345.3	180.2	276.0			
89.33117																	
147 51	.0 TDRS 171W	236.9	-53.7	94.9	180.1	6.0	.0	339.5	14.0	36.1	279.3	345.3	180.2	276.0			
89.37751																	
99.72243	23.10065 157.7819H 89.32535																
147 57	.0 PLATFORM ALINE	235.8	-42.6	124.4	180.1	342.8	359.9	339.5	14.0	36.1	279.3	345.3	359.8	267.2	0		
89.54282																	
148 12	.0 MNVR TO LVLH ATT FOR NV-1 OPS AND EO-7/8 OPS	231.8	1.9	162.0	.0	.0	180.0	243.7	304.9	86.4	282.2	12.6	.0	90.0			
89.38776																	
148 45	.0 MNVR TO INERTIAL	235.5	39.1	-62.1	90.0	.0	.0	239.2	34.8	139.8	357.0	17.3	.0	270.0			

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ATT FOR SLEEP

89.35034																	
151 0	.0	BEGIN SLEEP PERIOD	236.4	-49.5	63.5	90.3	359.9	162.0	239.2	34.8	139.8	356.9	17.4	89.5	72.0		
89.51653																	
159 0	.0	END SLEEP PERIOD	232.4	-9.0	-10.2	90.3	358.5	218.0	239.2	34.8	139.8	356.6	17.5	272.5	52.0		
89.35608																	
160 9	.0	TORS 41W	236.3	-52.8	-135.0	91.7	.4	124.7	239.2	34.8	139.8	356.6	17.5	90.5	34.7		
89.35608																	
160 9	.0	TORS 171W	236.3	-52.8	-135.0	91.7	.4	124.7	239.2	34.8	139.8	356.6	17.5	90.5	34.7		
89.33117																	
67.47160	96.03570	27.06258	115.92986														
160 15	.0	PLATFORM ALINE	236.9	-54.2	-97.2	91.8	357.7	147.9	239.2	34.8	139.8	356.6	17.5	89.5	57.9	C	
87.54342																	
161 30	.0	START PAYLOAD CLOSEOUT	231.8	-23.8	155.9	90.9	1.7	78.0	239.2	34.8	139.8	356.5	17.5	91.8	348.0		

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APPENDIX D: RESULTS OF STAR TRACKER CONSTRAINT VIOLATIONS  
ANALYSIS FOR PRELIMINARY BASELINE REFERENCE  
MISSION 1 USING PLATFORM ALINEMENTS IN THE  
INERTIAL HOLD MODE AT AN INITIAL LVLH ATTITUDE  
OF 0, 0, 0 \*

\* Included are printouts of Alpha ( $\alpha$ ) + 20° for Earth pointing constraint violations, printed after each event; and Angles Theta ( $\theta$ ) for Star Trackers 1 and 2 and the Sun, Star Tracker 3 and the Sun, Star Trackers 1 and 2 and the Earth, and Star Tracker 3 and the Earth, printed in a set of four numbers prior to each Platform Alinement.

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PRELIMINARY BASELINE REFERENCE MISSION 1  
SHUTTLE ATTITUDE AND POINTING TIME LINE  
WITH STAR TRACKER CONSTRAINTS INDICATED

APPENDIX D  
Page 1 of 3

GET HRS MN SECS	EVENT	VEHICLE POSITION			LVLH ATTITUDE			ECI ATTITUDE			LOOK ANGLES TO SUN		LOOK ANGLES TO EARTH		LOOK ANGLES TO TARGET		
		ALT N MI	LAT DEG	LONG DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	ROLL DEG	YAW DEG	PITCH DEG	YAW DEG	PITCH DEG	TARG ID	YAW DEG	PITCH DEG
0 45 55.5	MNVR TO ATT FOR ORB INSERTION	152.8	-29.4	74.2	359.8	13.1	.0	248.3	6.0	298.4	194.3	352.7	180.0	283.1			
93.23810																	
1 30 .0	BEGIN ON-ORBIT OPERATIONS	152.8	29.3	-121.2	180.1	350.7	180.0	248.3	6.0	298.4	194.3	352.8	360.0	80.7			
93.23769																	
3 0 .0	BEGIN SLEEP PERIOD	152.8	29.3	-143.9	179.9	350.8	180.0	248.3	6.0	298.4	194.4	352.8	.0	80.8			
93.23775																	
10 30 .0	END SLEEP PERIOD	152.8	29.3	102.5	178.7	351.5	179.9	248.3	6.0	298.4	194.6	353.1	.4	81.5			
93.28035																	
11 24 .0	TDRS 41W	152.0	-23.9	-51.2	.0	.0	.0	287.3	344.0	294.5	204.6	311.0	.0	270.0	311.8	59.7	
93.28035																	
11 24 .0	TDRS 171W	152.0	-23.9	-51.2	.0	.0	.0	287.3	344.0	294.5	204.6	311.0	.0	270.0	184.6	325.5	
93.33013																	
158.73898	71.00446 180.00000 90.00000																
11 30 .0	PLATFORM ALINE	151.1	-14.9	-29.1	.0	.0	.0	311.3	335.5	286.1	228.8	291.3	.0	270.0	8		
93.23809																	
12 0 .0	INITIATE TUG DEPLOYMENT	152.8	29.3	79.7	.0	.0	.0	74.9	359.4	241.0	343.5	15.0	.0	270.0			
93.28902																	
12 11 9.0	TUG SEPARATION	151.9	21.0	125.6	.0	.0	.0	115.5	19.4	248.0	330.1	56.5	.0	270.0			
93.25559																	
12 40 .0	INITIATE LOS ATT	152.5	-27.2	-132.9	.0	.0	.0	237.1	10.1	297.3	196.1	4.3	.0	270.0			
93.23849																	
27 0 .0	BEGIN SLEEP PERIOD	152.8	29.3	-147.5	177.8	341.3	180.0	237.1	10.1	297.3	196.4	4.8	.1	71.3			
93.30793																	
35 0 .0	END SLEEP PERIOD	151.5	-15.4	-152.5	4.3	318.1	356.0	237.1	10.1	297.3	196.6	5.0	355.6	312.1			
93.30695																	
36 54 .0	TDRS 41W	151.5	-22.4	-78.0	.0	.0	.0	283.7	342.1	293.3	209.2	315.1	.0	270.0	352.7	40.8	
93.30695																	
36 54 .0	TDRS 171W	151.5	-22.4	-78.0	.0	.0	.0	283.7	342.1	293.3	209.2	315.1	.0	270.0	198.3	348.3	
93.36311																	
153.63131	66.01779 180.00000 90.00000																
37 0 .0	PLATFORM ALINE	150.5	-12.8	-56.4	.0	.0	.0	308.2	334.1	284.0	231.2	296.4	.0	270.0	8		
93.31887																	
48 54 .0	TDRS 41W	151.3	-21.6	100.0	.0	.0	.0	282.1	341.3	292.6	211.3	317.1	.0	270.0	175.9	308.1	
93.31887																	
48 54 .0	TDRS 171W	151.3	-21.6	100.0	.0	.0	.0	282.1	341.3	292.6	211.3	317.1	.0	270.0	19.9	351.9	
93.37779																	
151.20333	63.63648 180.00000 90.00000																
49 0 .0	PLATFORM ALINE	151.2	-11.8	121.4	.0	.0	.0	306.8	333.8	283.0	232.2	298.8	.0	270.0	8		
93.24220																	
51 0 .0	BEGIN SLEEP PERIOD	152.7	29.2	-150.9	179.8	60.2	180.1	306.8	333.8	283.0	232.2	298.9	180.1	29.8			
93.28259																	
59 0 .0	END SLEEP PERIOD	152.0	-17.2	-156.8	178.9	300.2	182.4	306.8	333.8	283.0	232.1	299.2	358.6	30.9			
93.33046																	
60 54 .0	TDRS 41W	151.1	-20.9	-82.0	.0	.0	.0	280.5	340.4	291.9	213.2	319.1	.0	270.0	358.9	37.7	
93.33046																	
60 54 .0	TDRS 171W	151.1	-20.9	-82.0	.0	.0	.0	280.5	340.4	291.9	213.2	319.1	.0	270.0	201.4	352.0	
93.39191																	
148.76187	61.24009 180.00000 90.00000																

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APPENDIX D	
Page 2 of 3	
61 0	0 PLATFORM ALINE 149.9 -10.8 -60.8 .0 -.0 .0 305.5 333.3 281.9 233.1 301.2 .0 270.0 8
93.34169	
72 54	0 TDRS 41W 150.9 -20.0 95.9 .0 .0 .0 279.0 339.6 291.1 215.1 321.2 .0 270.0 181.8 310.7
93.34169	
72 54	0 TDRS 171W 150.9 -20.0 95.9 .0 .0 .0 279.0 339.6 291.1 215.1 321.2 .0 270.0 22.9 348.2
93.40545	
146.30842	58.83363 180.00000 90.00000
73 0	0 PLATFORM ALINE 149.7 -9.8 117.0 .0 -.0 -.0 304.2 332.8 280.8 233.9 303.7 .0 270.0 8
93.24853	
75 0	0 BEGIN SLEEP PERIOD 152.6 28.8 -154.3 179.9 60.1 180.2 304.2 332.8 280.8 233.9 303.8 180.1 29.9
93.25729	
83 0	0 END SLEEP PERIOD 152.5 -19.0 -160.9 179.1 300.8 182.2 304.2 332.8 280.8 233.8 304.1 358.7 30.8
93.35256	
84 54	0 TDRS 41W 150.7 -19.2 -86.1 -.0 -.0 .0 277.5 338.7 290.3 216.9 323.2 .0 270.0 4.5 34.4
93.35256	
84 54	0 TDRS 171W 150.7 -19.2 -86.1 -.0 -.0 .0 277.5 338.7 290.3 216.9 323.2 .0 270.0 204.2 355.7
93.41835	
143.84460	56.42236 180.00000 90.00000
85 0	0 PLATFORM ALINE 149.4 -8.7 -65.2 -.0 .0 -.0 303.0 332.4 279.6 234.6 306.2 .0 270.0 8
93.36303	
96 54	0 TDRS 41W 150.5 -18.3 91.9 .0 .0 .0 276.1 338.0 289.4 218.6 325.3 .0 270.0 187.1 313.5
93.36303	
96 54	0 TDRS 171W 150.5 -18.3 91.9 .0 .0 .0 276.1 338.0 289.4 218.6 325.3 .0 270.0 25.5 344.5
93.43058	
141.37226	54.01178 180.00000 90.00000
97 0	0 PLATFORM ALINE 149.2 -7.6 112.6 .0 -.0 -.0 301.8 332.1 278.4 235.3 308.6 .0 270.0 8
93.24094	
98 0	0 BEGIN SLEEP PERIOD 152.8 -20.1 -28.4 180.0 300.1 180.2 301.8 332.1 278.4 235.3 308.7 359.9 30.1
93.43926	
106 0	0 END SLEEP PERIOD 149.0 -6.8 -24.1 .3 359.3 1.3 301.8 332.1 278.4 235.2 309.0 61.0 271.5
93.37311	
108 54	0 TDRS 41W 150.3 -17.4 -90.1 .0 .0 .0 274.7 337.2 288.5 220.2 327.4 .0 270.0 9.6 30.9
93.37311	
108 54	0 TDRS 171W 150.3 -17.4 -90.1 .0 .0 .0 274.7 337.2 288.5 220.2 327.4 .0 270.0 206.7 359.6
93.44211	
138.89338	51.60782 180.00000 90.00000
109 0	0 PLATFORM ALINE 149.0 -6.5 -69.6 -.0 -.0 -.0 300.7 331.7 277.2 235.8 311.1 .0 270.0 8
93.38276	
120 54	0 TDRS 41W 150.1 -16.4 87.8 -.0 .0 -.0 273.3 336.5 287.6 221.7 329.6 .0 270.0 191.9 316.4
93.38276	
120 54	0 TDRS 171W 150.1 -16.4 87.8 -.0 .0 -.0 273.3 336.5 287.6 221.7 329.6 .0 270.0 27.8 340.7
93.45289	
136.41014	49.21693 180.00000 90.00000
121 0	0 PLATFORM ALINE 148.8 -5.4 108.2 .0 -.0 .0 299.5 331.5 275.9 236.3 313.6 .0 270.0 8
93.21700	
122 0	0 BEGIN SLEEP PERIOD 153.2 -21.8 -32.2 180.0 300.1 180.1 299.5 331.5 275.9 236.3 313.6 359.9 30.1
93.46051	
130 0	0 END SLEEP PERIOD 148.6 -4.6 -28.5 .2 359.3 1.3 299.5 331.5 275.9 236.2 313.9 62.5 271.5
93.39197	
132 54	0 TDRS 41W 149.9 -15.4 -94.2 .0 .0 .0 272.0 335.8 286.6 223.1 331.8 .0 270.0 14.0 27.2
93.39197	
132 54	0 TDRS 171W 149.9 -15.4 -94.2 .0 .0 .0 272.0 335.8 286.6 223.1 331.8 .0 270.0 208.7 3.6
93.46289	